

Studies on Less Rare-Earth Permanent Magnet Hybrid Excitation Motor with High Power Density

Takashi Kosaka, Nobuyuki Matsui

Omohi College, Graduate School of Engineering, Nagoya Institute of Technology

TEL/FAX: +81-52-735-5420, Email: kosaka@nitech.ac.jp

Abstract :

Feasibility studies on Hybrid Excitation Motor (HEM) as a candidate of less rare-earth permanent magnet and high power density machine for hybrid electric vehicle drive applications are reported. The basic working principle of the HEM is explained from a viewpoint of its variable field control mechanism. After making the design restrictions and the target specifications clear, the drive performances of a full-sized HEM designed as the motor with the maximum power of 123kW are predicted based on 3D-FEA using JMAG-Studio. Comparisons between the measured and the computed drive characteristics of the downsized test HEM demonstrates that the 3D-FEA based design and performance predictions have reasonable computation accuracy. As a result, it is concluded that the predicted performance of the full-sized machine, its high power density with 3.35kW/kg at the maximum power operation under utilization of 517g rare-earth permanent magnet, is highly expected.

JMAGUsers Conference 2010

Studies on Less Rare-earth and High Power Density Hybrid Excitation Motors

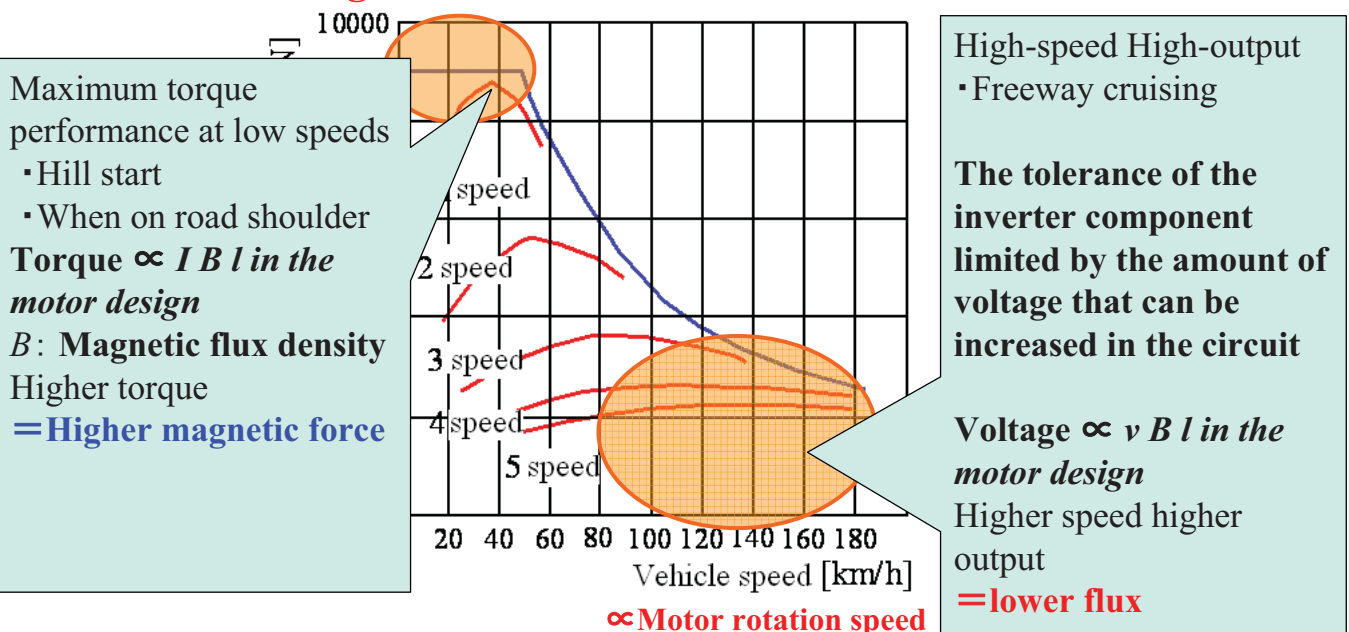
Takashi Kosaka and Nobuyuki Matsui

Graduate School of Engineering, Omohi College
Nagoya Institute of Technology
December 9, 2010 (Thurs)



1. Requirements and Design Challenges of Motors for EV/HEV

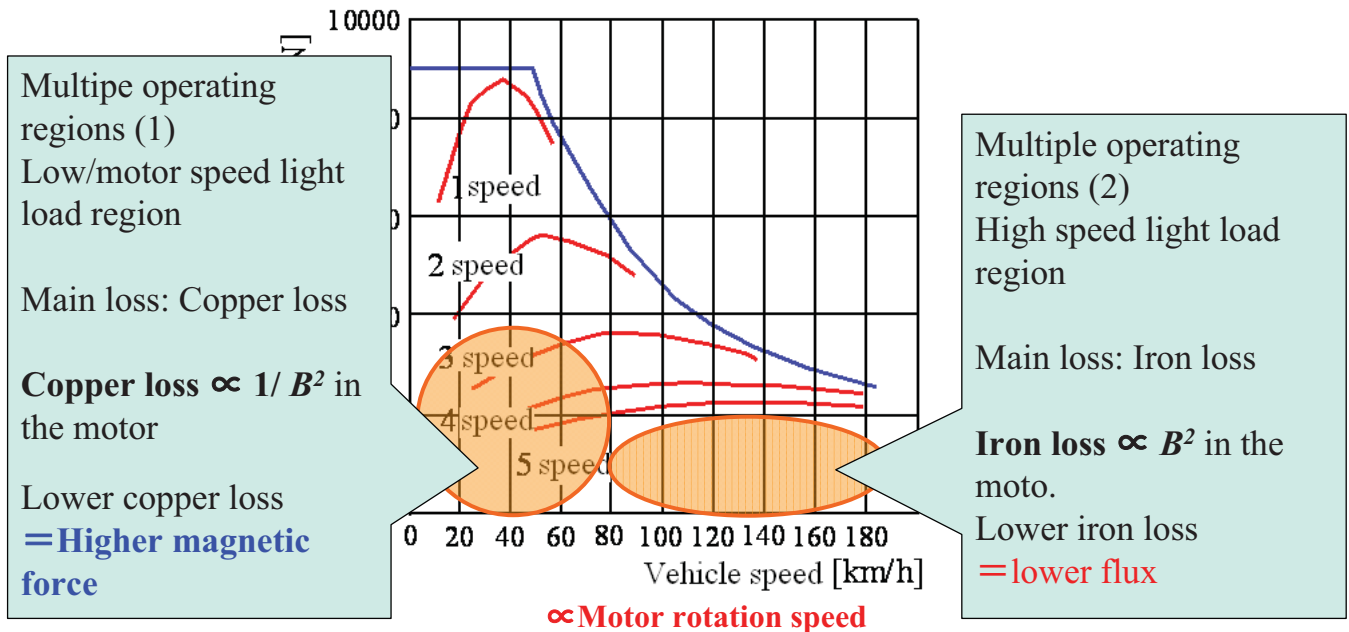
Wide range of speed - Covering the operation range of torque with a single miniaturized motor.





1. Requirements and Design Challenges of Motors for EV/HEV

Covering a wide range of operating drive regions efficiently with a single motor



2. Development Trends of Variable Magnetic Flux Motors

Variable Magnetic Flux

○2009: Toshiba Home Appliance Corporation Nikkei Electronics March 8, 2010 Issue 3

Switching Coil Connection

○2009: YASKAWA ELECTRIC CORPORATION July Nikkei AT2010

○2009: Hitachi Appliances Nikkei Electronics March 8, 2010 Issue 3

Combining magnetic force of permanent magnets and electromagnets \Rightarrow Hybrid magnetic motors

○1995: MEIDENSHA CORPORATION, IEEJ Vol.115-D, No.11, pp.1402-1411

○2003: Univ. of Wisconsin, Madison(USA)

IEEE Trans. on IA, vol. 39, No.6, pp. 1704-1709, 2003

○2007: SATIE - Ecole Normale Supérieure de Cachan (France)

Proc. of the 12th EPE 2007



3. Variable Flux Hybrid Magnetic Motor and Rare Earth

1. Rare earth for controlling magnetic force strengthening –

Magnetic force of magnets + Magnetic force of electromagnetics

If the magnetic force, B, necessary for low speed torque and light load low loss is 1:

Only magnet excitation --- **Magnetic force of magnets 1**

⇒Magnet ratio 100%

Hybrid excitation --- **Magnetic force of the magnets 0.5** + magnetic force of the electromagnets

0.5 ⇒Magnet ratio 50%

2. High-speed High Output under battery voltage constraints by controlling magnetic flux weakening

Lower loss higher efficiency --- Magnetic force of the magnets — Magnetic force of the electromagnets

Back EMF caused by eliminating magnetic force, B, and eliminating loss (iron loss)

Hybrid excitation --- **Magnetic force of the magnets 0.5** — **Magnetic force of the electromagnets 0.5**

⇒ No magnetic force

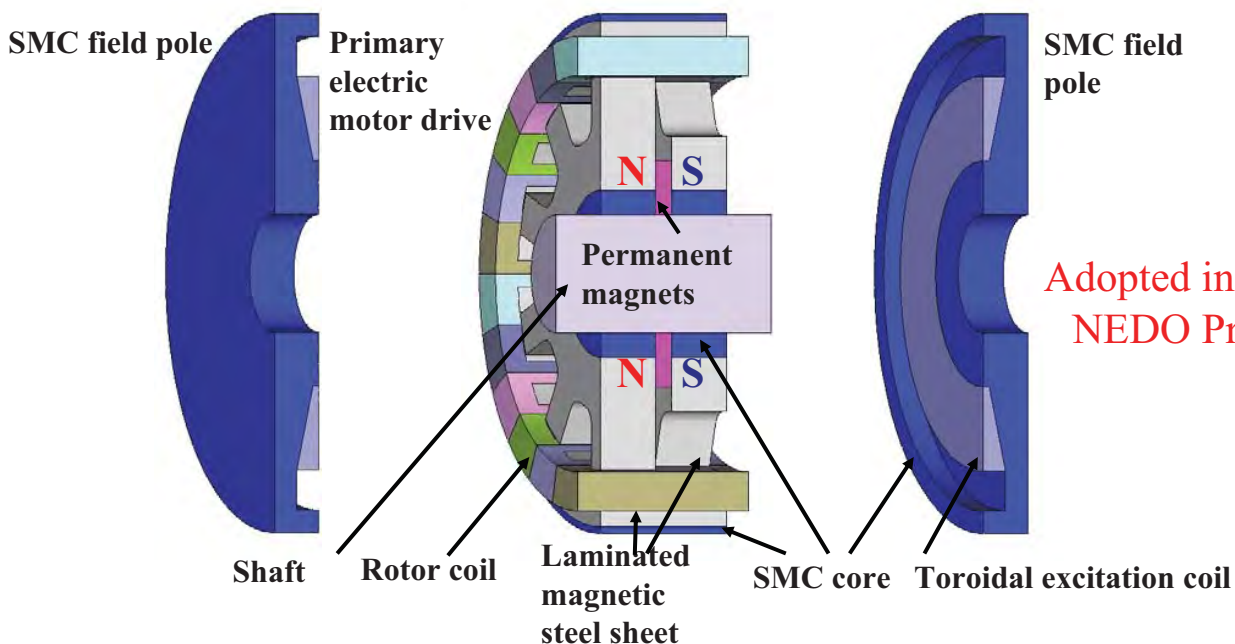
Challenges

Constructing a motor structure that efficiently utilizes both the magnetic force of the magnets and electromagnets.

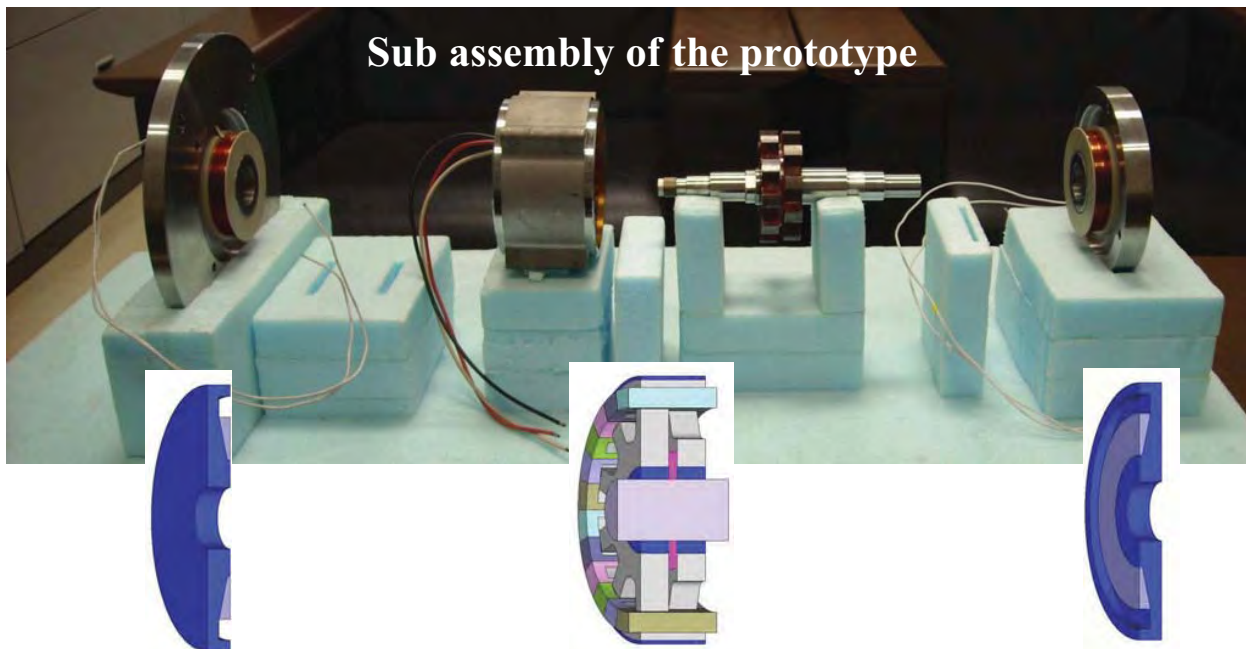


4. Rare earth hybrid excitation motor for HEVdrives

20-pole 24-slot concentrated winding hybrid excitation motor



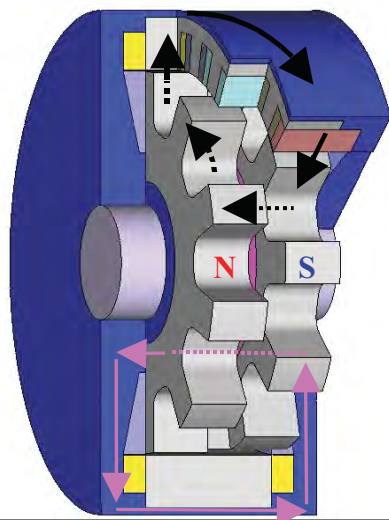
4. Rare earth hybrid excitation motor for HEVdrives



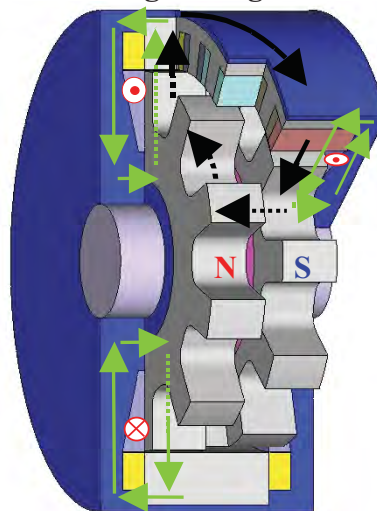
4. Rare earth hybrid excitation motor for HEVdrives

Operating Principles - Controlling Magnetic Flux Strengthening

<Excitation without control>



<Excitation with magnetic flux strengthening control>



Magnetic flux of permanent magnets + $T_m = P_n (\phi_m + \phi_f) i_q$
excitation magnetic flux



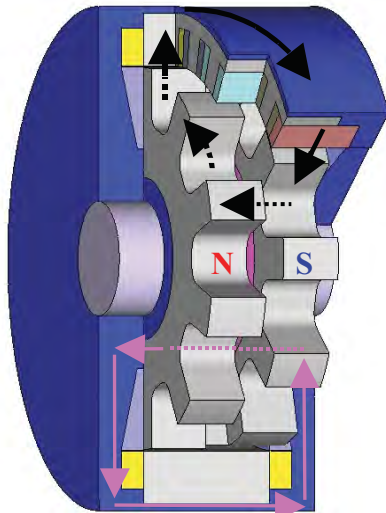
Higher torque by increasing the excitation magnetic flux



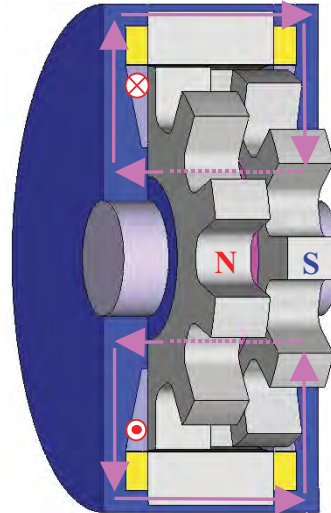
4. Rare earth hybrid excitation motor for HEVdrives

Operating Principles - Controlling Magnetic Flux Strengthening

<Excitation without control>



<Excitation with magnetic flux weakening control>



DC short circuit in the magnetic flux of permanent magnets
Reduces the flux linkage of the stator coil

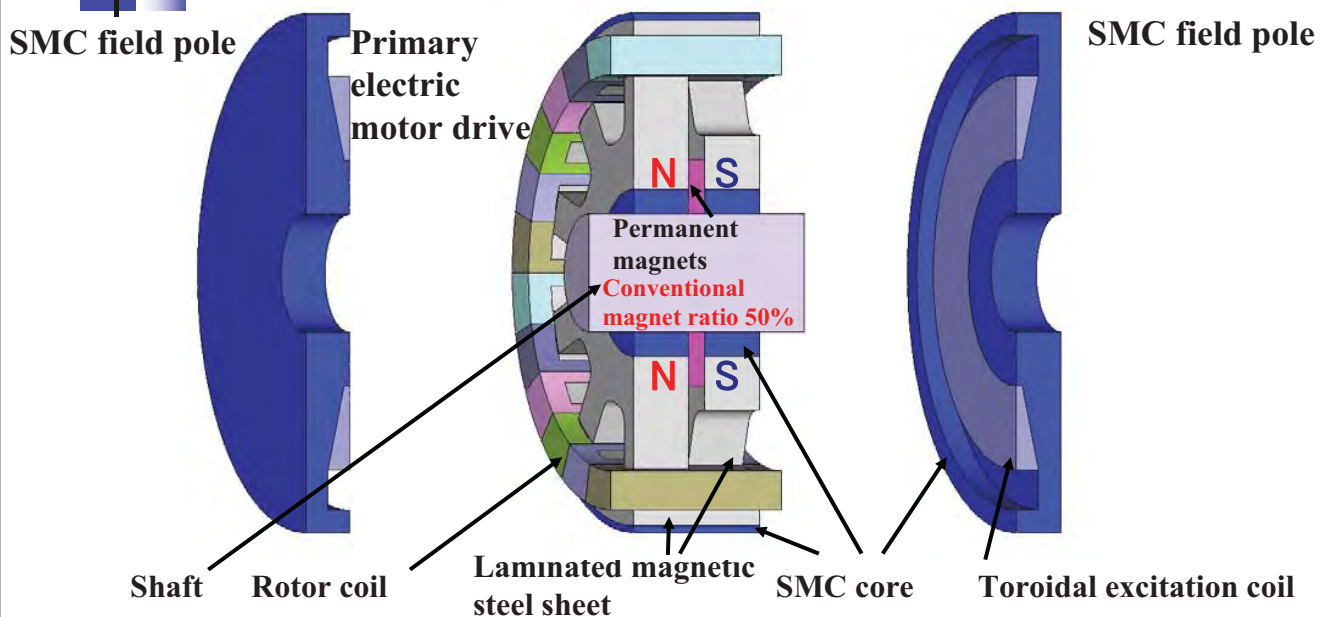


Lowers iron loss at high rotation speeds

Enlarging the speed range by controlling the back EMF



4. Rare earth hybrid excitation motor for HEVdrives



Rotor structure: Flat cylindrical magnets and laminated electromagnetic steel

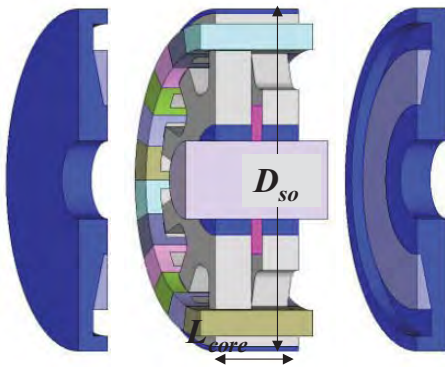
➡ Higher output via **higher rotation speeds**

Stator structure: Concentrated windings in multi-pole slots

➡ Higher winding factors and higher torque



5. Design Specifications of Motors for HEV Drives



Dimensions of the primary motor tested*

Stator diameter D_{so} : ϕ 264mm

Stack length of stator/rotor core L_{core} : 70 mm

Characteristics of primary drive motors for automobiles

- (1) Uses Neodymium magnets
- (2) Controlling magnetic field weakening – highly efficient at high speeds
- (3) Controlling magnetic field strengthening – Higher torque at low speeds
- (4) Compact & robust structure

Current density of rotor winding:

20[Amps/mm²] (standard water cooled)

Maximum inverter voltage:

650[V_{dc}](Present standard)

Magnet dimensions:

Outer Diameter : 115 mm

Inner diameter (shaft) : 60 mm

Thickness : 9 mm

Amount used: 68 cm³ (517 g)



5. Design Specifications of Motors for HEV Drives

<Design constraint conditions>

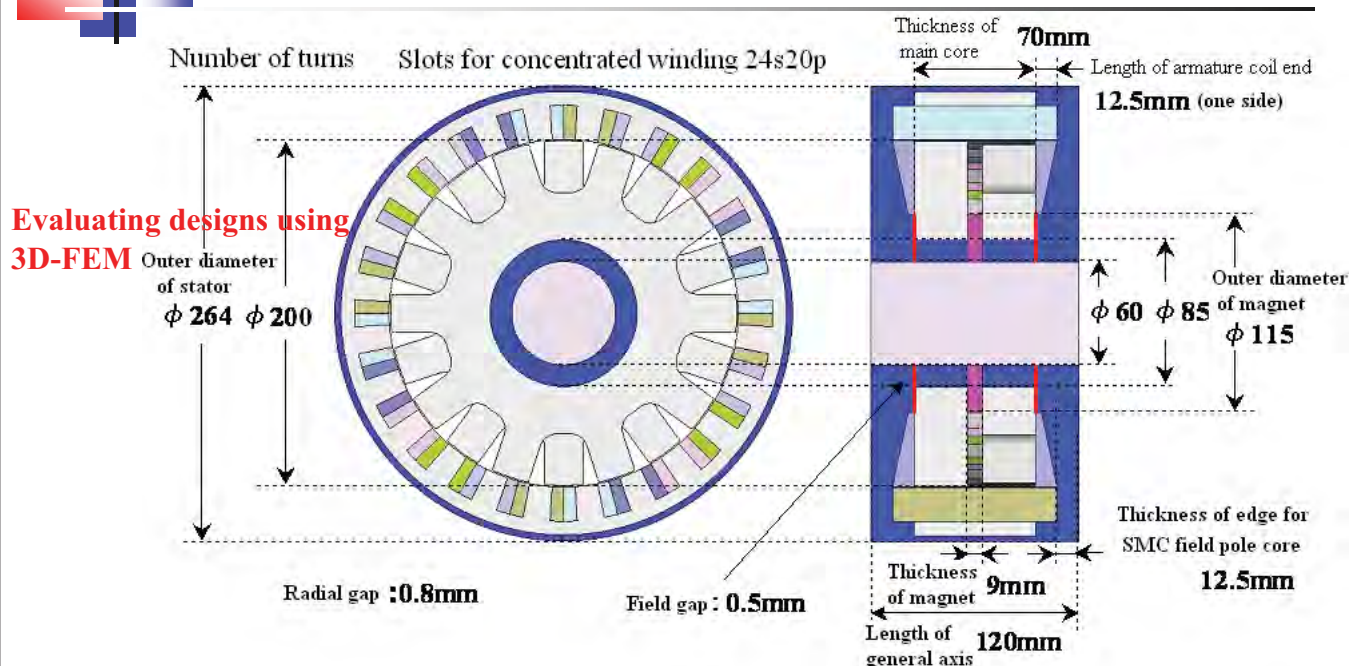
Motor diameter	264 [mm]	Magnets	< 550 [g]
Stack length of primary core	70 [mm]	Maximum inverter current	240[A _{rms}]
Maximum current density (Stator coil)	20 [A _{rms} /mm ²]	Inverter DC _{max} voltage	650 [V]
Maximum current density (Excitation coil)	20 [DCA/mm ²]	Maximum component tolerance	900 [V _{0-p}]

<Performance specifications>

Max. speed	20,000 [r/min]		
Max torque	More than 210 [Nm]	Desired torque density	More than 6 [Nm/kg]
Maximum output	More than 123 [kW]	Desired output density	More than 3.5 [kW/kg]



6. Estimating 3D-FEA Design Geometry and Performance

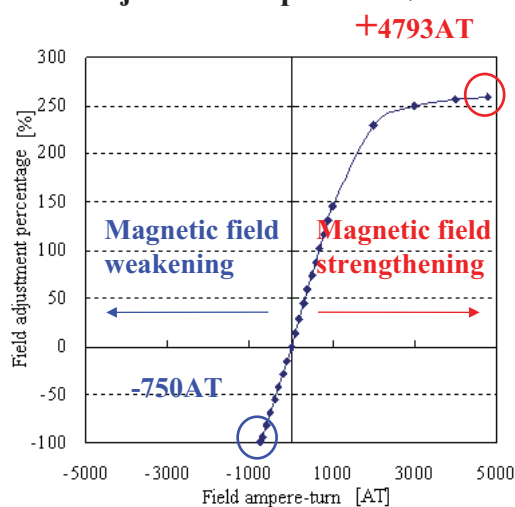


I.Ozawa, et.al, "Less Rare-Earth Magnet-High Power Density Hybrid Excitation Motor Designed for Hybrid Electric Vehicles Drives", Proc. of 13th European Conference on Power Electronics and Applications (EPE2009), No.772(2009)

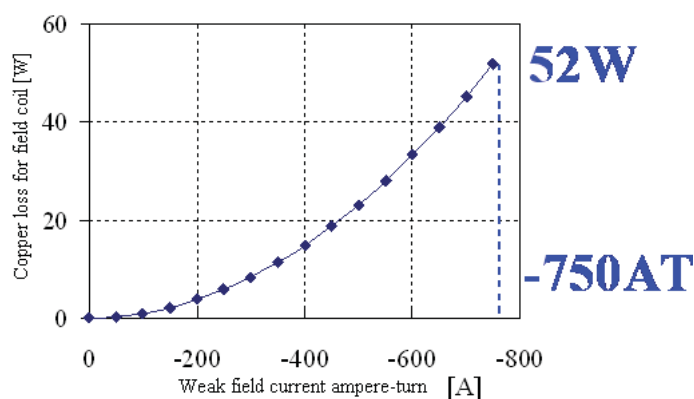


6. Estimating 3D-FEA Design Geometry and Performance

<Magnetic field weakening/strengthening adjustment capabilities>



<Copper loss of excitation winding at -750AT>

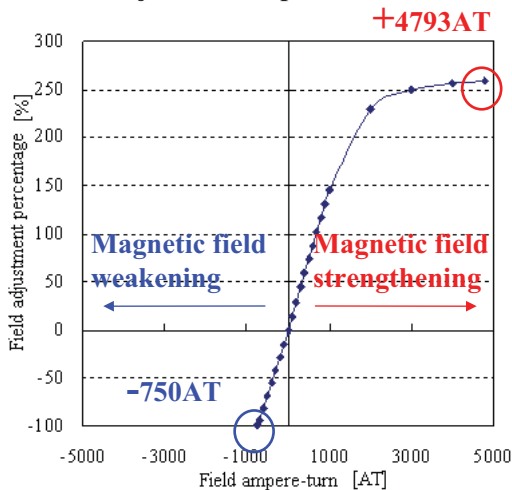


Weakening -100%~ Strengthening +258%



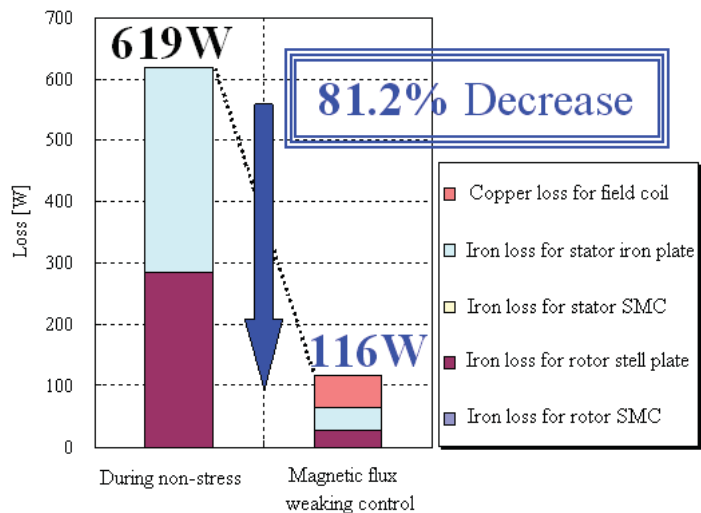
6. Estimating 3D-FEA Design Geometry and Performance

<Magnetic field weakening/strengthening adjustment capabilities>



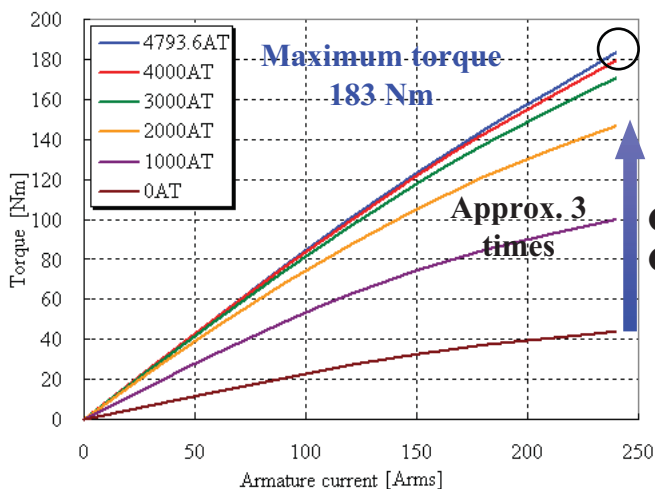
Weakening -100%~ Strengthening +258%

<Dragging iron loss at 20,000 r/min>



6. Estimating 3D-FEA Design Geometry and Performance

<Stator current vs. torque characteristics>



43Nm@240Arms — 0AT

146Nm@240Arms — 2,000AT

Copper loss of rotor coil 3.25 kW @ 240 Arms
Copper loss of excitation coil 0.49 kW @ 2,000 AT

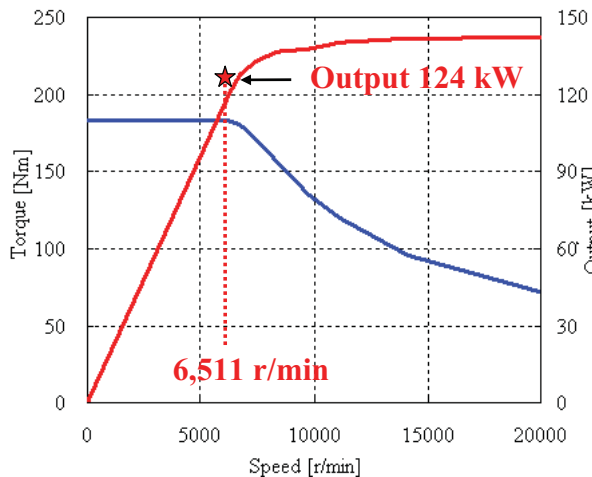
(with a coil temperature of 100 degrees Celsius)

Max. torque: 183 Nm (87.1% of desired value) rotor torque density: 83.6 Nm/L
Excitation magnetic force 2,000 AT=0.5 kWcopper loss with 3 times the torque constant up

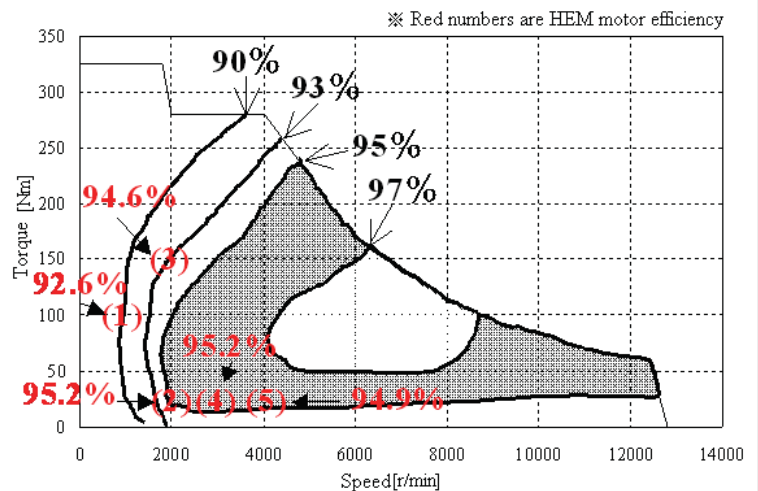


6. Estimating 3D-FEA Design Geometry and Performance

<Rotation speed vs. torque & output characteristics>



<Motor efficiency at multiple operating points>



Maximum output: **124 kW @ 6,511 r/min PF = 0.65** The desired output is achieved

Output density: $124 \text{ kW}/37.0 \text{ kg} = 3.35 \text{ kW/kg}$ (97.1% of desired output density)



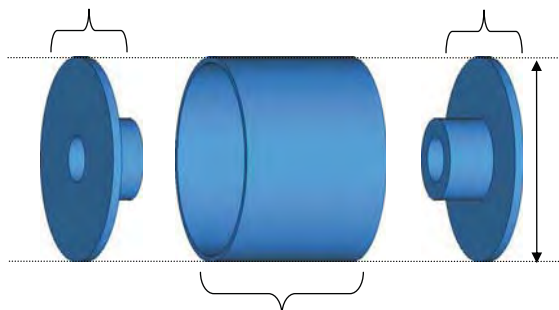
7. Evaluating the Performance of Miniaturized Prototype Testing

○Scale down limitations - Size of SMC materials

Excitation pole SMC core

Excitation pole SMC core

Universal SMC cylindrical material
(Material from Mistubishi PMGMBS318)



Outer circumference of SMC stator core

Full scale
 $\phi 264 \text{ mm}$

$\phi 100 \text{ mm}$

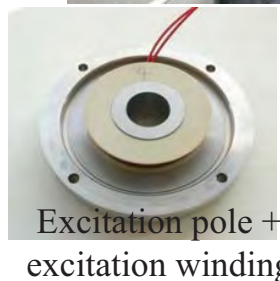
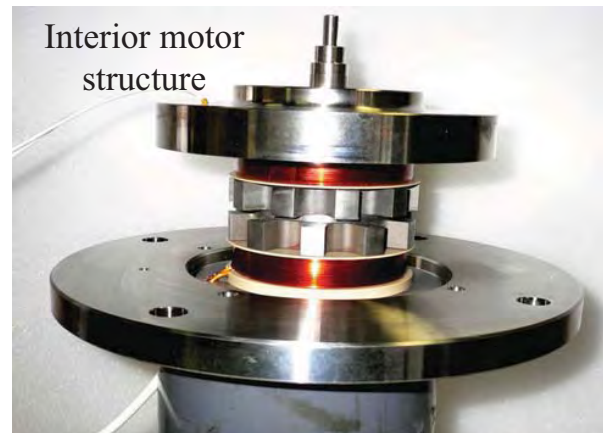
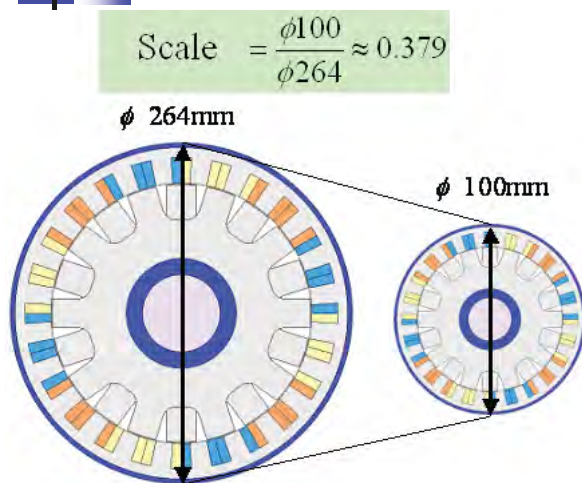
$L=50 \text{ mm}$

Scaling ratio $k=100/264=0.378\dots$ approx. the same scale of dimensions

—Radial air gap $0.8 \times k=0.303 \div 0.3 \text{ mm}$

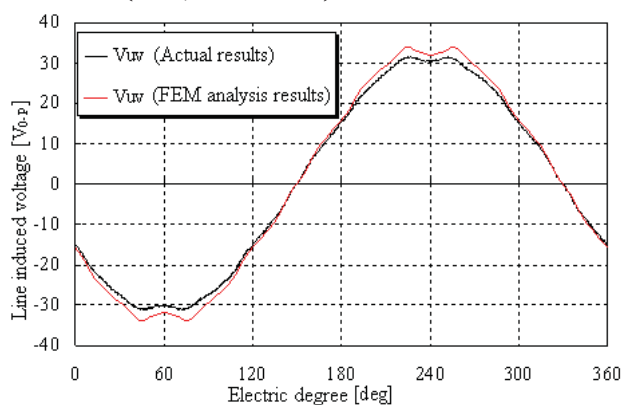
—Excitation gap $0.5 \times k=0.189 \div 0.2 \text{ mm} \Rightarrow 0.5 \text{ mm expanded (gap management)}$

7. Evaluating the Performance of Miniaturized Prototype Testing

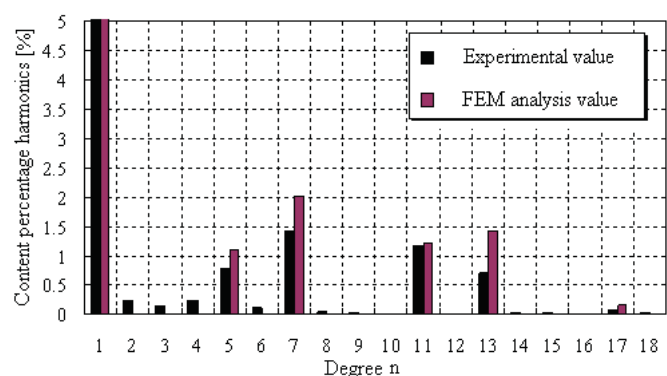


7. Evaluating the Performance of Miniaturized Prototype Testing

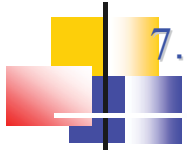
<Back EMF waveform between wires
(at 3,000 r/min)>



<Rate including harmonic components>

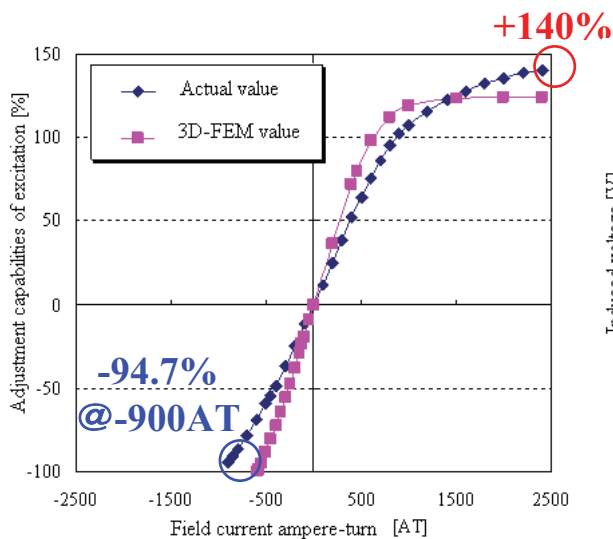


The error between the actual results and FEM analysis results is - 6.6%(at 3,000 r/min)
The harmonic components of the back EMF waveform match well

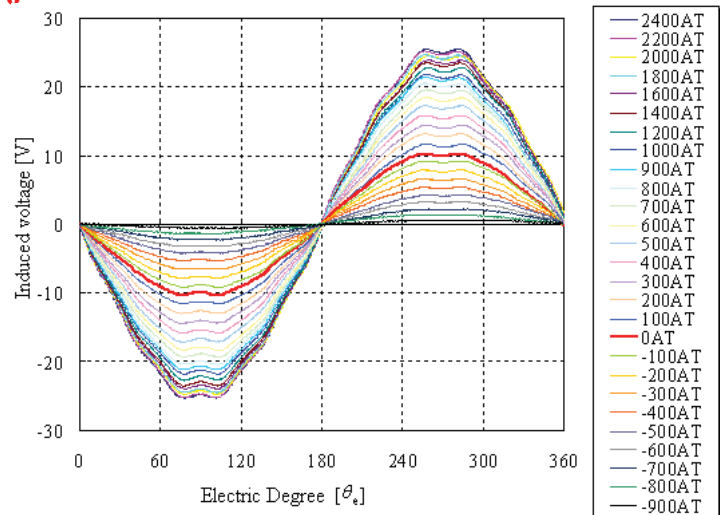


7. Evaluating the Performance of Miniaturized Prototype Testing

<Adjustment capabilities of excitation>

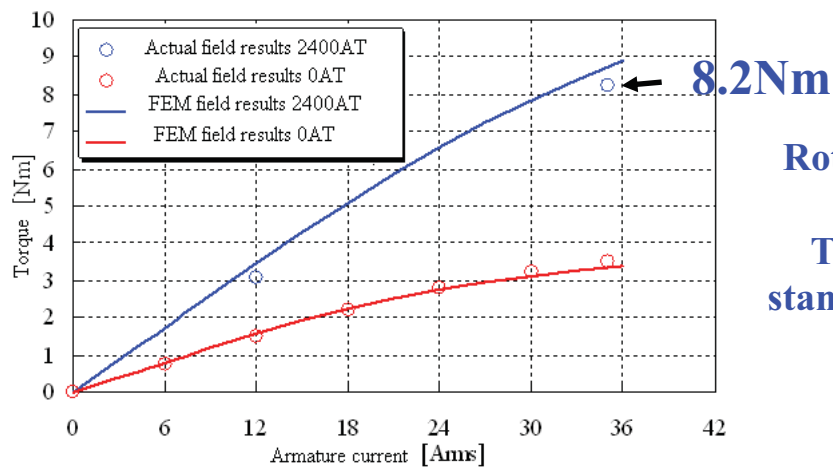


<Back EMF waveform between wires (at 1,000 r/min)>



7. Evaluating the Performance of Miniaturized Prototype Testing

<Rotor current - Torque characteristics (at 1,000 r/min)>



Rotor torque density
68.8 Nm/L
Testing an 82.3%
standard of 83.6 Nm/L

Actual maximum torque 8.2 Nm
Estimated FEMtorque 8.8 Nm

Estimated error -7%

Accuracy of evaluating performance by 3D-FEM \Rightarrow Realizing full scale features High



8. Conclusion

- Uses Neodymium magnets : Compared to conventional technology: 50 [%] — 500 [g] approximately
- Torque mass density : Equal to conventional technology — 6 [Nm/kg]
- Output mass density : Equal to conventional technology — More than 3.5 [kg/kW]
(Note: Water cooled type motor)
- Maximum speed : 20,000 r/min (Compatible to conventional maximum torque of a 4:1 gear)

Achieved in the full scale design (JMAG estimate from full 3D-FEA calculation)

Desired performance	Desired value	Design results	Achievement
Amount of magnetic material used	Approx. 500 [g]	517 [g] (NEOMAX38AH)	OK
Maximum speed	20,000 [r/min]	Voltage limitations and mechanical intensity cleared	OK
Max torque	More than 210 [Nm]	183 [Nm]	87%
Output @ 6-7 kr/min	More than 123 [kW]	124 [kW] @ 6.5kr/min	101%
Desired torque density	More than 6 [Nm/kg]	4.9[Nm/kg]	81.6%
Desired output density	More than 3.5 [kW/kg]	3.35 [kW/kg]	97.1 [%]